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OXYGEN AND pH MICROPROFILES ABOVE CORRODING MILD STEEL COVERED WITH A BIOFILM

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 O_2 and pH microprofiles were measured above corroding mild steel covered with a biofilm. The pH in the anodic areas (tubercles) ranged from 5 to 7 and was always 9.45 at the surface of the cathodic areas. After 1 month of biofilm development, O_2 was depleted at the anodic area but could reach the cathodic surface where it was reduced. Consequently, differential O_2 concentration cells were the driving force for corrosion. The O_2 microprofiles indicated that O_2 was consumed in the tubercles, probably by microbial activity, while O_2 was reduced electrochemically in the cathodic areas. It was concluded that O_2 transfer to the cathodic surface was the rate limiting step for the corrosion process.

KEYWORDS: biofilm, corrosion, microelectrode, tubercle, mild steel

INTRODUCTION

Mild steel, commonly used in the industrial water systems, is prone to corrosion. The corrosion products, deposited on the steel surface, consist of three layers of iron oxides at different stages of oxidation, viz. ferrous hydroxide (Fe(OH)₂), hydrous ferrous ferrite (Fe₃O₄.nH₂O) and hydrous ferric oxyhydroxide (FeOOH.H₂O) (Uhlig, 1971; Misawa, 1973). The general corrosion rate is determined by the rate of O₂ reduction. Since O₂ is transported from the bulk liquid through the porous layers of corrosion products to the steel surface, corrosion rates are limited by 1) the O₂ consumption rate by microbial activity in the layer of corrosion products and the biofilm covering the steel surface and/or 2) the diffusional resistance in the layer of corrosion products (Bonnel *et al.*, 1983). Passivation of mild steel occurs at very high O₂ concentrations, but does not take place under air saturated conditions (Uhlig, 1971). In its initial stage, corrosion of mild steel is a localized process but eventually involves the whole surface (Szklarska-Smialowska, 1986).

The most dangerous form of localized corrosion of mild steel is tuberculation. According to Herro (1991), tubercle formation originates from a differential O₂ concentration cell. Local O₂ depletion can occur under a non-uniform biofilm. O₂ reduction occurs in the cathodic area and produces hydroxyl ions, while in the anodic area (the tubercle) iron dissolution occurs. Due to hydrolysis by Fe²⁺ and formation of Fe(OH)₂, protons are formed, leading to a low pH within the tubercle. The Fe²⁺ generation prompts an anion flux into the tubercle to maintain electro-neutrality. Pitting corrosion beneath the tubercle is suggested to be a transport controlled process (Butler & Ison, 1966), whose rate is determined by the ion mobility through the corrosion products. The present objective was to verify this mechanism in the presence of microorganisms by

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measurement of O₂ and pH microprofiles with microelectrodes at cathodic areas and within tubercles covered with biofilm.

Ideal microelectrodes have small tip diameters to prevent distortion of the local environment, small sensor surfaces for optimal spatial resolution, low noise levels, a stable signal, high selectivity and should be strong enough to resist breakage during the measurements. The relatively rigid cathode type O₂ microelectrodes are suitable for measurements on solid surfaces (Revsbech, 1983). No ideal pH electrode is available at the present time. Different types of pH microelectrodes have been used for microprofile determinations in sediments (Revsbech & Jorgensen, 1986) and in biofilms from bioreactors (de Beer et al., 1993; de Boer et al., 1993). Full glass pH microelectrodes are highly selective, but have a large sensor surface, with a length of at least 30 μ m (Thomas, 1978; Revsbech & Jorgensen, 1986). Metal iridium oxide microelectrodes are sturdy and have a low noise sensitivity, enabling measurements in reactors (VanHoudt et al., 1992), but their signal is influenced by Fe⁺² and S⁻², and the iridium oxide layer may detach upon touching a solid surface, leading to an unstable signal. The signal of liquid membrane microelectrodes is hardly influenced by interfering substances. However, due to their small size the electrodes are fragile and very sensitive to noise. The maximum tip diameter is about 3 μ m, larger capillaries lose their membrane easily because of the lower capillary force. For pH determinations at steel surfaces covered with partially anaerobic biofilm liquid membrane microelectrodes are preferred, because of their insensitivity to Fe²⁺ and S²⁻. The behavior of larger, and thus stronger, liquid membrane microelectrodes was tested, with membranes stabilized by solidification.

EXPERIMENTAL

Detailed descriptions of the experimental system and operating conditions are presented in previous papers (Lee *et al.*, 1993a,b; Nielsen *et al.*, 1993). Mild steel coupons were placed in a closed flow channel reactor with a recirculation loop to provide sufficient mixing. The average flow velocity was 0.3 m·s⁻¹. The reactor was operated as a continuous flow reactor at a dilution rate of 0.4 h⁻¹. Twenty four corrosion coupons (AISI 1018 mild steel, 15.9 mm diameter) were mounted into the bottom of the reactor. The temperature was controlled at 30°C. The medium consisted of 0.35 g·1⁻¹ artificial seawater (Instant Ocean, aquarium Systems, Mentor, OH), 1.0 mg·1⁻¹ sodium lactate,

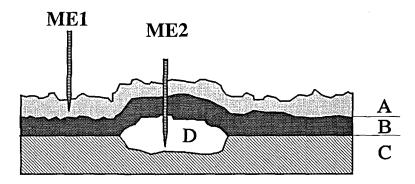


Fig. 1 Schematic diagram of corroding mild steel. A = the biofilm; B = the layer of corrosion product; C = the metal; D = the pit below the tubercle. Also shown are microelectrodes positioned in the cathodic area (ME1) and in the pit below the tubercle (ME2).

1.0 mg·l¹ NH₄Cl, and 20 mg·l¹ Na₂HPO₄. The pH in the bulk was 7.5 and the bulk O_2 concentration was 0.25 mol·m³. *Pseudomonas aeruginosa, Klebsiella pneumonia*, and *Desulfovibrio desulfuricans* were used as inocula but the reactor was not run aseptically. Microprofile measurements were performed after 1 month of biofilm development. The diameters of the tubercles then ranged from 1–3 mm. The tubercles covered *ca* 20% of the metal surface. A schematic representation of a tubercle is given in Figure 1.

Microelectrodes

A cocktail was prepared containing 12% hydrogen ionophore II, 2% potassium tetrakis (4-chlorophenyl)borate, 60% 2-nitrophenyl octyl ether, 22% poly-vinyl chloride (high molecular weight) and 4% cellulose acetate. The cocktail was dissolved in approximately 5 volumes of tetrahydrofuran (THF). All chemicals were obtained from Fluka Chemical Corporation, New York. Glass tubing of 5 mm diameter was drawn in a flame to capillaries 1 mm thick. Subsequently, microtips were drawn using an automatic vertical puller (model 51217, Stoelting Company). The tip was opened by careful pushing against a glass rod using a micromanipulator, resulting in a final tip diameter of 5-10 μ m. The tips were silanized by dipping in 5% trimethylchlorosilane in carbon tetrachloride for 15 s, followed by baking at 175° C for 10 min. The electrode tips were filled with sensor by dipping the tips in the cocktail. After filling, the electrodes were left overnight in a dust free container at room temperature to let the THF evaporate, leaving a solid pH sensitive membrane in the tip. The electrode shaft were filled with 50 mM sodium phosphate buffer (pH 7.0) supplemented with 300 mM KCl. Electrical connection was made with a Ag/AgCl wire. The electrode potential difference with an Ag/AgCl reference electrode was measured with a Keithley 617 electrometer. Calibration of the microelectrodes was performed in a buffer containing 50 mM sodium phosphate, 50 mM sodium citrate and 50 mM sodium borate. The buffer was titrated with 1 M HCl or 1 M NaOH and the microelectrode signal was compared with the pH of the solution measured with a normal glass pH macroelectrode. Iridium oxide pH microelectrodes and cathode type O2 microelectrodes were prepared and calibrated as described previously (Revsbech, 1983; VanHoudt et al., 1992).

Microprofile Measurements

The microelectrodes were mounted on a motor-driven micromanipulator with a 1 μ m accuracy. Corroding coupons were removed from the channel reactor and mounted in a polycarbonate batch reactor (1 × w × h = 10 × 10 × 3 cm), so that their surface was flush with the reactor bottom. The reactor liquid was obtained form the channel reactor and sparged with air in one of the corners for aeration and circulation of the reactor liquid. The biofilm surface was determined optically, while the steel surface was determined as the position where bending of the electrodes occurred. Additionally, O_2 and pH profiles were determined in the channel reactor, using O_2 and iridium oxide pH microelectrodes.

RESULTS AND DISCUSSION

The PVC-solidified liquid membrane remained firmly attached in the tip of relatively large microelectrodes with tip diameters of 5–10 μ m. Membranes without PVC addition disappeared during filling of the shaft with electrolyte. The electrodes were more sturdy than those of microelectrodes with 1 μ m tips and remained intact after touching a solid

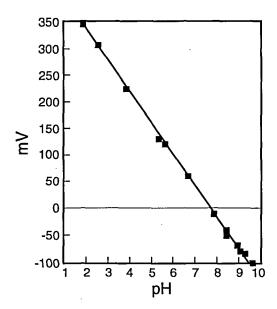


Fig. 2 Calibration curve of pH microelectrode with solidified liquid membrane.

surface. The response of the microelectrodes to pH values in the range of 1.5 to 9.5 was linear with slopes of 50–58 mV/pH (Fig. 2). The response time (t₉₀) was approximately 1 s. The signal drifted less than 3 mV·h during measurements. The calibration line was not influenced by addition of 20 mM Na₂S or 10 mM FeSO₄. Their mechanical strength and high selectivity coefficients enabled measurements near a mild steel surface covered with a biofilm containing sulfate-reducing bacteria. However, the design of the microsensor may be improved to reduce to noise sensitivity, *e.g.* by encasing the shaft in metal or inserting the electrode in another capillary filled with KCl as a shielding. At present, its use is restricted to areas with low noise levels such as a Faraday cage.

Microprofiles Measured in the Batch Cell

The pH values on the mild steel coupon surface were strongly influenced by the presence of tubercles as shown by pH microprofiles in the batch reactor. The microprofiles around the tubercle (cathodic site) consistently showed a pH increase ranging from pH 7.5–8.0 in the bulk liquid to 9.5 on the steel surface (Fig. 3). Profiles measured above tubercles (anodic site) were more variable but always showed a pH decrease in the direction toward the tubercle surface (Fig. 3). The pH values on the surface of the tubercles ranged from 5 to 7. The high pH value on the cathodic site and the low pH value toward the anodic site can be explained by corrosion reactions. During the tubercle formation, hydroxyl ions are generated at the cathodic site by O_2 reduction. The hydroxyl ions combined with ferrous ions migrating from the anodic site to form $Fe(OH)_2$. The ferrous hydroxide layer forms a diffusion barrier for O_2 and other reactants. The pH value of a saturated $Fe(OH)_2$ solution is 9.45, a value measured at the steel surface in the cathodic zones. The acidity within the tubercle is caused by the hydrolysis of ferrous or ferric ions and persists because of the restricted mass transfer imposed by a porous cap of corrosion products. The irregular

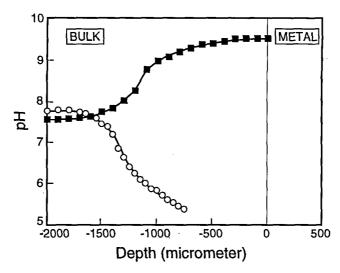


Fig. 3 pH profiles measured above corroding mild steel covered with a 1 mm thick biofilm. ○-○ = profiles measured above a 0.75 mm thick tubercle; = = profiles measured above the cathodic area between the tubercle. Microprofiles were recorded down to the solid surface but the microelectrode did not penetrate the tubercle.

occurrence of cracks in the tubercle resulted in variable permeability. Therefore, pH concentrations showed a greater variation above the tubercle than around the tubercle areas.

The significant differences in pH on the surface of a corroding mild steel offer an opportunity for monitoring pitting corrosion. Tubercles can be detected by their low pH value. Instead of using pH microelectrodes, detection with pH indicator dyes may be a more attractive alternative for routine measurements.

 O_2 microprofiles showed consumption both on anodic and cathodic sites. The concentration at the cathodic surface was usually close to 0.05 mol·m³, but some measurements showed surface concentrations of 0.0 mol·m³ (Fig. 4). The O_2 microprofiles above the cathodic area consisted of two or three almost perfectly linear parts (Fig. 4). O_2 can be consumed by microbial activity in the biofilm and by electrochemical reduction at the steel surface. Lactate was the sole carbon source and assuming microbial lactate oxidation was the only O_2 consuming process, the O_2 concentration in the biofilm was calculated as follows

$$C_O = C_{BO} - Y(C_{Blac}) \left(\frac{D_{lac}}{D_O}\right) \tag{1}$$

where C_0 is the local O_2 concentration, Y the moles of O_2 necessary to oxidize one mole of lactate (Y = 3), C_{BO} the O_2 bulk concentration, C_{Blac} is the lactate bulk concentration and D_{lac}/D_O is the ratio of the diffusion coefficients of lactate and O_2 . A value for D_{lac} of $1.05 \times 10^{9} \,\mathrm{m^2 \, s^{-1}}$ was calculated using the Wilke-Chang equation (Treybal, 1981) and O_0 was $2.33 \times 10^{9} \,\mathrm{m^2 \, s^{-1}}$ (Andrussow, 1969). From the bulk liquid concentrations of lactate (less than $10^{-2} \,\mathrm{mol \, m^{-3}}$) and O_2 (0.25 $\mathrm{mol \, m^{-3}}$), it was calculated that the lowest possible O_2 concentration in the biofilm will be 0.236 $\mathrm{mol \, m^{-3}}$ if microbial lactate oxidation was the only oxygen consuming process. The measured O_2 concentrations in the biofilm were much lower, therefore, microbial O_2 consumption by substrate from the bulk was

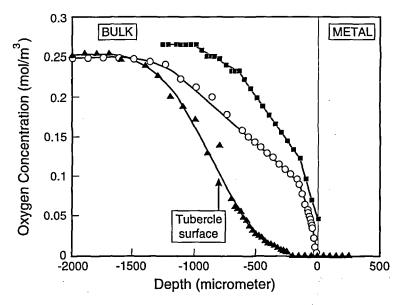


Fig. 4 O_2 profiles measured above the same mild steel surface as in Figure 3. $\triangle - \triangle =$ profiles measured above a tubercle; $\bigcirc - \bigcirc$ and $\blacksquare - \blacksquare =$ profiles measured above cathodic areas. The microelectrode could penetrate the tubercle and reach the pit.

insignificant in the cathodic region. Alternatively, microbial Fe2+ oxidation might occur above the cathodic area. However, Fe²⁺ oxidising bacteria are acidophilic (Schlegel, 1981) while the local pH is high. Moreover, the linearity of the O₂ microprofiles indicate negligible O₂ consumption by the biofilm covering the steel surface. The shape of the microprofiles is consistent with the explanation that O₂ was almost exclusively reduced electrochemically at the cathodic site. The differences in the gradients of the linear parts indicate the existence of multiple layers with different diffusivities covering the steel surface. Since the O₂ fluxes below and above the deflection points were equal, the ratio of the O2 gradients was equal to the ratio of the diffusion coefficients. It was estimated that the O₂ diffusion coefficient in the outermost layer was 3 to 10 times higher than in the adjacent layer closer to the steel surface. In a number of experiments a second deflection point was observed, indicating the existence of a third layer adjacent to the steel surface. with a lower diffusion coefficient than the two upper layers. In these experiments complete depletion of O₂ at the steel surface was found. Probably, the bottom layer was relatively dense and could not always be penetrated by microelectrodes. The layer covering the cathodic areas, probably consisting mainly of corrosion products and biofilm, decreased the O₂ flux towards the surface, thereby reducing the corrosion rate.

The O_2 profile above the tubercles showed more variation and the tubercle surface concentration ranged from 0.1–0.2 mol·m³. The irregularity was probably due to turbulent hydrodynamics caused by the uneven tubercle surface and by cracks in the tubercle. When the O_2 microelectrode could penetrate through a crack into the tubercle, lower O_2 concentrations were detected and non-linear profiles within the tubercle were recorded (Fig. 4), typical for matrices with active microorganisms. The O_2 profile measured down tot he bottom of the pit showed depletion 250 μ m above the steel surface. The shape of the profiles can be explained by a flux of reducing species, such as H_2 , S^2 or $Fe^{2\tau}$, diffusing

from the bottom of the pit towards the bulk liquid. Consequently, microbial population above a tubercle can feed on different substrates and may have a different composition than above cathodic areas, which grow only on substrates from the bulk liquid.

Microprofiles Measured in the Channel Reactor

The solidified liquid membrane microelectrode appeared too noise-sensitive for measurements in the channel reactor and the electrode could only be used in the batch reactor. Although the medium was the same in both systems, the pH profiles could be different due to different flow regimes. To examine whether the pH profiles measured in the batch reactor are representative for profiles occurring in the channel reactor, O₂ profiles were measured in both experimental systems and compared. O₂ profiles measured on the same coupon, first in the channel reactor, then in the batch cell, were similar (data not shown), demonstrating comparable hydrodynamics. This was further supported by pH profiles measured in the channel reactor with an iridium oxide microelectrode, showing a pH increase to pH 9 at the surface of the cathodic zone and a pH decrease to pH 6 at the surface of a tubercle (data not shown). It was concluded that the pH profiles in the batch reactor were identical to those in the channel reactor.

CONCLUSIONS

The pH was 9.45 at the cathodic surface and 5–7 at the tubercle surface. O_2 was depleted above the anodic sites but could reach the cathodic surface, where it was reduced. Differential O_2 concentration cells were the driving force for the corrosion process. O_2 transfer to the cathodic surface was the rate limiting step, due to mass transfer resistance in the layer of corrosion products and biofilm covering the cathodic area.

References

Andrussow, L. (1969) Diffusion. In: Landolt-Bornstein Zahlenwerte und Functionen II/5a. Springer, Berlin, pp 513-727.

Bonnel A, Dabosi F, Deslouis C, Duprat M, Keddam M, Tribollet B J (1983) Corrosion study of a carbon steel in natural chloride solutions by impedance techniques. *J Electrochem Soc* 130: 753–766

Butler G, Ison HCK (1966) Corrosion and its Prevention in Waters. Reinhold, New York, pp 45-46.

de Beer D, van den Heuvel J C, Ottengraf S P P (1993) Microelectrode measurements of the activity distribution in nitrifying bacterial aggregates. Appl Environm Microbiol 59: 573-579

de Boer J P, Cronenberg C C H, de Beer D, van den Heuvel J C, Teixeira de Mattos M J, Neijssel O M (1993) pH and glucose profiles in aggregates of *Bacillus laevolacticus*. Appl Environm Microbiol **59**: 2474–2478

Herro H M (1991) Tubercle formation and growth on ferous alloys. *Corrosion '91, NACE*, Houston, Texas, Paper No 84.

Lee W, Lewandowski Z, Okabe S, Characklis W G, Avci R (1993a) Corrosion of mild steel underneath aerobic biofilms containing sulfate-reducing bacteria Part I: at low dissolved oxygen concentration. *Biofouling* 7: 197-216

Lee W, Lewandowski Z, Morrisen M, Characklis W G, Avci R, Nielsen P H (1993b) Corrosion of mild steel underneath aerobic biofilms containing sulfate-reducing bacteria Part II: at high dissolved oxygen concentration. *Biofouling* 7: 217-239

Misawa, T. (1973) The thermodynamic consideration for Fe-H₂O system at 25°C. Corros Sci 13: 659-676

Nielsen P H, Lee W, Lewandowski Z, Morrisen M, Characklis W G (1993) Corrosion of mild steel in an alternating oxic and anoxic biofilm system. *Biofouling* 7: 267–284

Revsbech N P (1983) In situ measurement of oxygen profiles of sediments by use of oxygen microelectrodes. In: Graigner E, Forstner H (eds) Polarographic Oxygen Sensors: Aquatic and Physiological Applications. Springer, Heidelberg

Revsbech N P, Jorgensen B B (1986) Microelectrodes: their use in microbial ecology, Adv Microbial Ecol 9:

293-352

Schlegel H G (1981) Allgemeine Mikrobiologie. Thieme Verlag, Stuttgart, pp 345-346

Szklarska-Smialowska Z (1986) Pitting corrosion of metals. Corrosion '86, NACE, Houston, Texas pp 3-5

Thomas R C (1978) Ion-selective Intracellular Microelectrodes. How to Make and Use them. Academic Press, London

Treybal R E (1981) Mass Transfer Operations. 3th edition, McGraw-Hill

Uhlig H (1971) Corrosion and Corrosion Control: an Introduction to Corrosion Science and Engineering. 2nd Edition, Wiley & Sons, New York, pp 91–126.

VanHoudt P, Lewandowski Z, Little B (1992) Iridium oxide pH microelectrode. Biotechnol Bioeng 40: 601-608