

POWER MANAGEMENT FOR MICROBIAL FUEL CELLS

by

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ABSTRACT

Monitoring parameters characterizing water quality, such as temperature, pH and concentrations of heavy metals in natural waters, is often followed by transmitting the data to remote receivers using telemetry systems. Such systems are commonly powered by batteries, which can be inconvenient at times because batteries have a limited lifetime and have to be recharged or replaced periodically to ensure that sufficient energy is available to power the electronics. To avoid these inconveniences, we have designed and tested a self-renewable power source, a microbial fuel cell, which has the potential to eliminate the need for batteries to power electrochemical sensors used to monitor water quality and small telemetry systems used to transmit the data acquired by these sensors. To demonstrate the utility of the microbial fuel cell, we have combined it with low-power, high-efficiency electronic circuitry providing a stable power source for wireless data transmission. To generate enough power for the telemetry system, energy produced by the microbial fuel cell was stored in an ultracapacitor and used in short bursts when needed. Since powering commercial components of electronic circuits requires 5 Volts, and our cell was able to deliver a maximum of 2.1 V, we used a DC-DC converter to increase the potential. The DC-DC converter powered the transmitter, which gathered the data from the sensor and transmitted them to a receiver. To demonstrate the utility of the system, we initially measured temporal variations in temperature followed by the implementation of a chemical sensor to measure copper and lead concentrations in water; this data was then wirelessly transmitted to a remote receiver

CHAPTER 1

INTRODUCTION

Chemical sensors have become indispensable components of contemporary systems monitoring quality of natural waters such as concentrations of mercury and lead. Once a sensor is deployed and activated, a link to an external data storing device, such as a computer, is needed. The easiest way to connect these devices is to hardwire the sensor to a computer/data logger, but in many applications where the sensors are deployed in remote regions, such a solution is not practical and wireless communication is recommended.

Purpose

Recent advances in chemical sensors, electronics, and wireless data transmission have made it possible to monitor water quality remotely and transmit the data wirelessly using telemetry systems, and such systems have been successfully deployed and used. A telemetry system provides the means for transmission/recording of data over a certain distance. This transmission can be in the form of a wireless link or a hardwire connection. If the data transmission is made using radio frequency (RF) transmitters the system can be labeled a “Wireless Telemetry system”. Telemetry systems are used to transmit parameters from various

kinds of sensors. For example, chemical sensors combined with telemetry systems have been used to monitor heavy metals, such as copper and mercury (1-4); organophosphate nerve agents (5); phenolic compounds; (6) explosive 2,4,6-trinitrotoluene (TNT); and hydrazine (7). Chemical sensors have also been used to monitor blood glucose and oxygen concentrations in diabetes patients. Salehi *et al.* 1996 used a telemetry link to wirelessly transmit the measured parameters to a data logger. Such telemetry links have been used for human biomonitoring applications such as heart rate monitoring, blood pressure measurement and various other vital parameters (Budinger *et al.* 2003), and to monitor the heart rate and respiration rate of divers in under water environments (Istepanian *et al.* 2002). Telemetry systems were also popular in tracking movement and monitoring of large scale animals and lambs.

Although combining chemical sensors with telemetry systems is still mostly in the research phase, some sensors, such as temperature sensors, have been widely used in such configurations (8), to measure temperature remotely. Sensors that measure temperature, humidity, pressure changes, pH, wind speed etc. are readily available from specialized vendors such as Madgetech inc.

Typically, batteries are used to power chemical sensors and telemetry systems. In some applications where the telemetry system is deployed in remote places researchers have used solar power, wind power or piezoelectric fibers as alternative energy sources, each of which have their own advantages and disadvantages. The obvious disadvantages of solar and wind is the inconsistency of energy generation. In some applications replacing batteries can be costly, time consuming and impractical.

A possible solution to this problem is to use self-renewable power supplies such as microbial fuel cells, which can operate for a long time using local resources. Such a power supply is just an alternative, self sustaining power source like solar or wind power.

Microbial fuel cells cannot operate at extremely low temperatures because microbial reactions slow as temperature decreases. Currently, we do not know how the system behaves at low temperatures; this will require long-term testing. However, it is expected that when the temperature returns to a higher values, the rates of microbial reactions will increase, and the system would recover. We tested our system for over one year in the laboratory and in the field, stopped it abnormally to estimate the effect of interrupted power generation, and every time the system recharged the capacitor and started to transfer the data once the conditions of normal operation had been restored.

Microbial fuel cells offer many advantages over batteries as power sources because they require no recharging. The main problem with using microbial cells is the small amount of power produced by the cell, which may not be enough to run a sensor and a transmitter continuously. To some extent this problem can be solved by increasing the surface area of the electrodes. If it is not possible to increase the surface area, the system can be operated less frequently using a suitable power management program; data transmission occurs only when enough energy has been accumulated. Another advantage of the microbial fuel cell is that even when exposed to extreme conditions microbial fuel cells can spontaneously recover once these

conditions are removed. It is well known that regular batteries lose their efficiency permanently at very low temperatures, and do not recover when the temperature returns to normal (27).

Prior Research on Microbial Fuel Cells

A microbial fuel cell (MFC) can be defined as a system that uses microorganisms to catalyze metabolic or enzyme catalytic energy into electrical energy (Allen and Bennetto 1993). However most researchers have been hesitant to pursue this as a viable power option because the power generated by a MFC is minuscule compared to the other options stated. However for some environmental monitoring applications where the frequency of data acquisition is not a major requirement, MFC's can work out very well. Extensive research toward developing reliable microbial fuel cells is focused mostly on selecting suitable organic and inorganic substances that can be used as sources of energy (9). Examples of such studies: Kim *et al.* oxidized organics (such as glucose) (10), Liu *et al.* used various organic matter in wastewater (11), and Cooney *et al.* and DeLong *et al.* used microbially produced sulfide oxidation as an anodic reaction (12,13). While the number of possible anodic reactions in microbial fuel cells is practically limitless, the number of cathodic reactions available in microbial fuel cells is much and they often are abiotic reactions, such as oxygen reduction (10,11,14-16), ferricyanide reduction (10,17) and iron reduction (18).

Prior Research on Environmental Microbial Fuel Cells

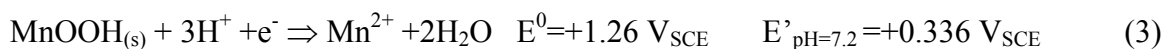
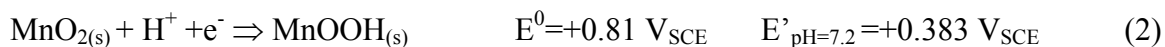
Looking for possible sources of energy for the microbial reactions in microbial fuel cells deployed in natural waters, some researchers have considered harvesting energy from marine and freshwater sediments. Reimers *et al.* and Tender *et al.* oxidized reduced substances in the marine bottom sediments near Tuckerton, NJ, U.S.A. and Raritan Bay, NJ, U.S.A. using graphite electrodes; they reduced oxygen on the cathode (19,20). Delong and Chandler proposed using microbial fuel cells deployed in the ocean to operate sensors, and suggested oxidizing microbially produced sulfide as the anodic reaction and reduction of oxygen as the cathodic reaction (13).

Proposed Environmental Microbial Fuel Cell

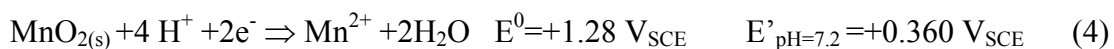
The microbial fuel cell we used in this study consisted of a sacrificial anode combined with the reduction of biomineralized manganese oxides. The sacrificial anode was a commercially available slab of a magnesium alloy composed of more than 99% magnesium; the remaining 1 % were other metals added to control the dissolution rate. The magnesium in the alloy dissolved according to the following reaction where E is the equilibrium potential:



As the cathodic reactants we used biomineralized manganese oxides, which are known to form on microbially colonized noble metals in natural waters. It has been demonstrated that biomineralized manganese oxides can affect the rates and the mechanisms of electrochemical reactions (21-23), leading to microbially influenced corrosion of metals. When corrosion coupons made of 316 L stainless steel were left immersed in a freshwater creek, the open circuit potential of the coupons increased from -50 mV to +400 mV_{SCE} (24-26). Shortly after being exposed to the creek water, the coupons were covered with biomineralized manganese oxide (MnO₂). Since the biomineralized manganese oxide was in direct electrical contact with the stainless steel, the metal exhibited the dissolution potential of MnO₂, as shown in the following reactions:



The overall reaction is:



The potentials were calculated assuming that the concentration of Mn²⁺ was 1 × 10⁻⁶ M. As a result of reaction 4, manganese oxides were reduced to divalent manganese, Mn²⁺, by electrons released from the dissolution of magnesium. However, since the Mn²⁺ ions were released within the biofilm of manganese-

oxidizing bacteria (MOB) covering the metal surface, the manganese-oxidizing bacteria reoxidized Mn^{2+} ions back to manganese oxides (21), thus forming a recyclable cathodic reactant. This mechanism can lead to a particularly pervasive form of microbially influenced corrosion of stainless steel, but can be also used as an efficient cathodic reaction in microbial fuel cells.

Hypothesis

It is our intent to demonstrate that a combined a sacrificial anode with microbial cathode can generate enough energy to power telemetry systems:

1. Powering an off-the-shelf thermocouple-based temperature sensor.
2. Powering a chemical sensor built by our research team to detect copper and lead in water.

Microbial fuel cells produce small amounts of energy and the goal of this study was to demonstrate that by implementing appropriate energy management program the energy generated by such fuel cells was adequate to power chemical sensors and telemetry systems, such as the one shown in figure 1.1. This study was carried out in two steps, the first of which showed that it was possible to use a microbial fuel cell to power a simple telemetry system which was a thermocouple-based remote temperature monitoring system. This temperature sensor was purchased from a specialized vendor and power management circuitry was designed to operate this simple sensor using a microbial fuel cell. The second

step implemented a custom-designed chemical sensor module that measures copper and lead concentrations in water. The power management circuitry that was used to power the temperature sensor in the first step was integrated into the design of the custom chemical sensor module. This chemical sensor module was then powered by a microbial fuel cell.

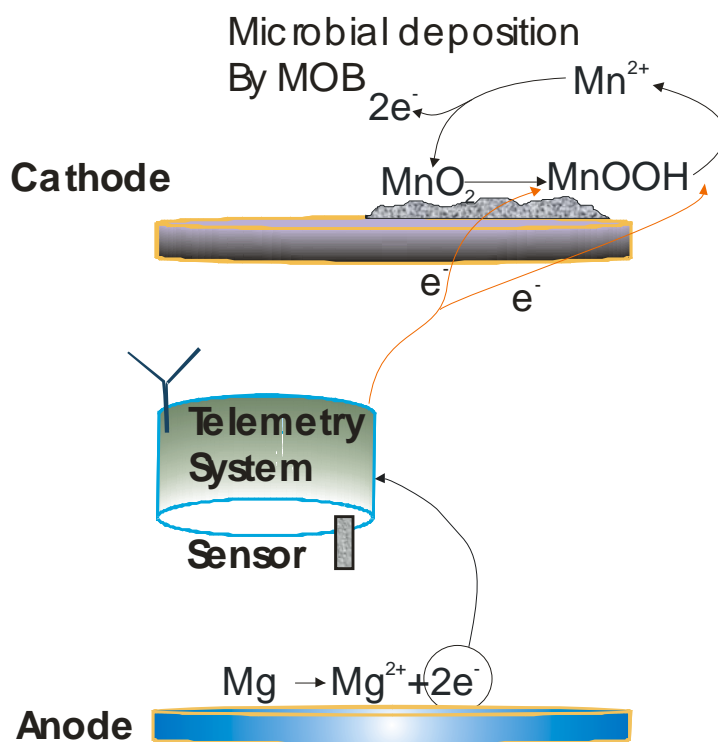


Figure 1.1. A sensor and a telemetry system powered by a microbial fuel cell.

Selecting appropriate anodic and cathodic reactions was the first step in the process of designing a system that could power the sensor and the telemetry system.

Before the utility of the device could be demonstrated, three problems had to be solved:

Problems Encountered

Problem #1: Storage of energy

Most solar energy powered systems use the energy generated by the solar panels to charge a battery pack which then powers the necessary devices. This kind of system is implemented because the amount of power generated by the solar panels can vary drastically depending on the intensity of sunlight and the use of battery packs can compensate for any peak power demands that might be forced on the system. A microbial fuel cell can be thought of in this same way as it cannot sustain the continuous operation of electronic devices. As a result the energy generated by the microbial fuel cell had to be accumulated in devices, such as capacitors, over a certain period of time and then delivered in short bursts to the sensor and telemetry system.

Problem #2: Increasing and controlling the electrical potential generated by the microbial fuel cell.

The main drawback of microbial fuel cells was that individual cells could not be connected in series like we would in batteries to increase the total overall potential. This is due to the fact that the electrodes are in the same solution (electrolyte), therefore when we connect them in series we are inherently shorting the anodes and

the cathodes leading to a drop in cell potential. Virtually all electronic components available on the market require working potentials higher than those delivered directly by microbial fuel cells. In addition, the potential of microbial fuel cells varies with time. Therefore, the potential developed by the microbial fuel cell needed to be stepped up and stabilized to power commercially available electronic components.

Problem #3: Restarting the system.

To ensure the sensor and the telemetry system did not drain the microbial fuel cell due to its high power consumption during operation, we made sure that the telemetry system was disconnected from the fuel cell until there was enough energy built up in the storage device for its operation. Because the energy was accumulated and delivered in short bursts, to generate adequate power, the system had two modes of operation: *sleep mode* and the *active mode*. Each time, before entering the active mode, the system had to be restarted. This required the implementation of a low power electronic device to monitor the voltage level of the energy storage device and to activate the required sensor electronics once there is sufficient energy built up.

Proposed Power Management System

The flowchart shown in figure 1.2 was the proposed power management system that was needed to run a telemetry system using an environmental fuel cell. The cathode is 316L stainless steel and the anode is a magnesium alloy. Next is an

energy storage device which in our case is a capacitor. The box labeled DC-DC converter boosts the input potential from the capacitor to a potential sufficient to power the transmitter and sensor which comprises the telemetry system

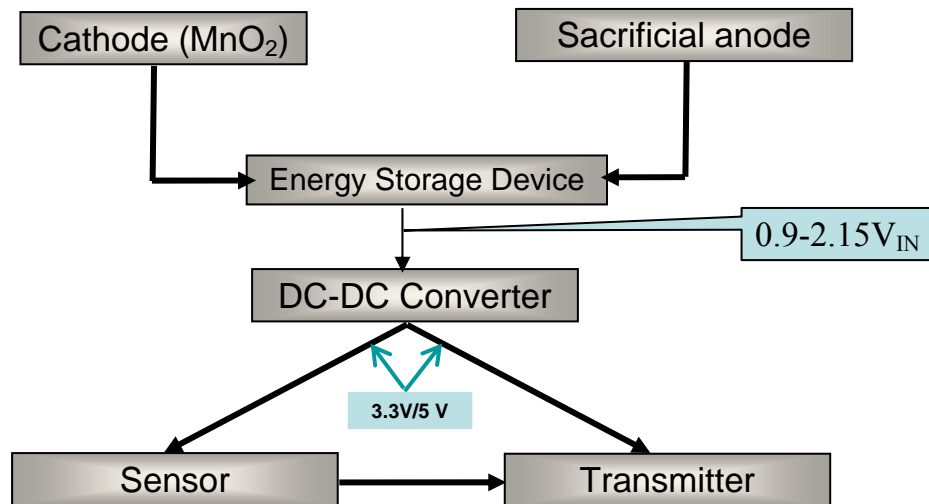


Figure 1.2. Power management system needed for an environmental microbial fuel cell

SOLUTIONS TO THE PROBLEMS

Problem #1

Storing electrical energy can be done in various ways, the most common being the use of batteries. Batteries have proven to provide suitable power levels for various applications. Problems such as shelf life and charge-discharge cycles of batteries have caused researchers to look for alternatives. Using rechargeable batteries may shorten the lifetime of the system because capacitors have a longer lifetime than rechargeable batteries (27). If we use a dry cell battery or a car battery to power the

sensor and the telemetry system, they will lose their charge with time, and cannot be used without recharging; their lifetime is controlled by maintenance requirements and by leakage current.

The development of high density capacitors known as ultracapacitors or electro-chemical capacitors work extremely efficient in certain applications. To solve the first problem, which was the accumulation of the energy generated by the microbial fuel cell, the energy produced by the microbial fuel cell was stored in an ultracapacitor. This had many advantages over using rechargeable batteries, such as a charge-discharge cycle life hundreds of thousands of times greater than that of the batteries. Also rechargeable batteries require the use of charging/discharging control circuitry making the system more complicated. The ultracapacitor we used had a rated lifetime of 10 yrs and a very low leakage current (about $0.28 \mu\text{A/h}$ at 25°C). Ultracapacitors have a much lower energy density storage capability compared to batteries; this is the determining factor in our decision to use ultracapacitors rather than batteries. When compared to regular capacitors which store energy by charge separation over two conducting plates separated by a dielectric, ultracapacitors store energy like a battery; it has two electrodes immersed in an electrolyte with a separator between the electrodes. The electrodes are very high in surface area. The charge is stored near the interface between the solid electrode and the electrolyte. A cross-section of a double-layer ultracapacitor is shown in figure 1.3.

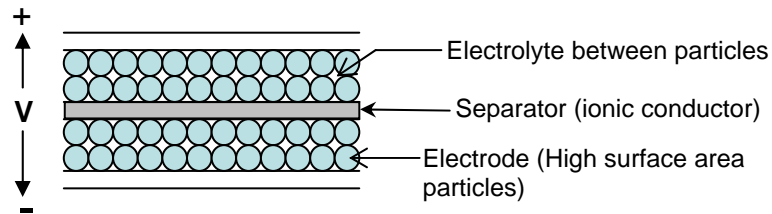


Figure 1.3. Cross-section of an ultracapacitor adapted from “Ultracapacitors: why, how and where is the technology”, Andrew Burke 2000

Problem #2

To solve the second problem, which was to increase and maintain the potential from the microbial fuel cell; we used a DC-DC converter to step up (boost) the potential of the microbial fuel cell. A DC-DC converter can be used to step up, step down or invert any input potential to a desired value. DC-DC converters use switching regulators to carry out the step up, step down (buck) or inverting (buck-boost) processes. A switching regulator is an electronic circuit which uses an energy storage device such as a capacitor, inductor or transformer to transfer energy from the input to output in discrete packets. A constant output voltage is maintained by the implementation of feedback circuitry. Depending on our need, switching regulators can be used to step up, step down or invert the output voltage (www.maxim-ic.com/appnotes.cfm/appnote_number/710). A simple step up switching regulator configuration is shown in figure 1.4.

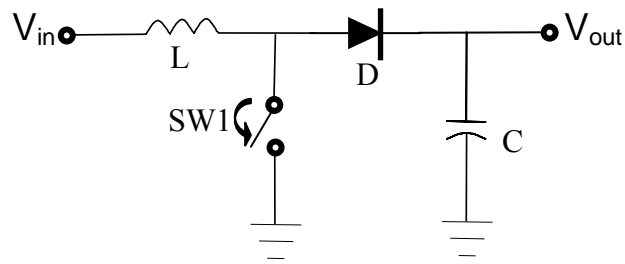


Figure 1.4. Basic configuration of a boost switching regulator

In figure 1.4, V_{in} is a constant input voltage source and V_{out} is the boosted voltage that is needed to run the necessary electronics. The part labeled L is an inductor, D is a diode and C is a capacitor. A switching regulator works by following these steps:

1. We can first assume that the switch (SW1) has been open long enough such that the capacitor is charged to the input voltage.
2. At $t=0$ the switch is closed and the input voltage is forced across the inductor resulting in a linear increase of current flow through the inductor. The diode prevents the discharge of the capacitor to ground.
3. When the switch is opened the current through the inductor decreases linearly over time and the inductor voltage increases enough to forward bias the diode. This allows the capacitor to charge up to a voltage higher than the input voltage. This process constitutes one charge-discharge cycle.
4. The voltage across the capacitor will keep rising with each cycle and with the implementation of feedback and control circuitry this output voltage can be controlled.

Such DC-DC converters that use switching regulators are readily available for various output and input voltage ranges. Since powering the electronic circuits used in the telemetry system requires a stable potential of 3.3 V for powering the temperature sensor and 5V for powering the custom chemical sensor, and our cell was able to deliver a maximum of 2.1 V. A DC-DC converter was used to increase and maintain the potential at the desired level. Once the potential was increased and kept at the desired level, the system controller powered the transmitter which acquired the data from the sensor and sent the data to a receiver. The receiver then logged the data onto a computer using a serial interface.

Problem #3

To solve the third problem, which was the need to restart the system once enough energy was accumulated in the ultracapacitor, we used a voltage comparator. The voltage comparator monitored the voltage level of the ultracapacitor and turned on the DC-DC converter when sufficient energy for transmission had been accumulated. A voltage comparator accepts two analog signals and produces a binary output (www.maxim-ic.com/appnotes.cfm/appnote_number/886). In our application of the input analog signal was compared with a reference voltage.

In situations that have a slow DC input signal it is sometimes recommended to implement hysteresis (positive feedback) to prevent the voltage comparator from entering multiple switching. Hysteresis works by pulling the input signal into the

comparator through the threshold when the output switches. This was however not implemented into our circuit design.

Applications

The designed power management system can be used to control a variety of sensors and telemetry systems powered by microbial fuel cells. The main principle of the power management system we used was that the energy generated by the fuel cell was stored in the ultracapacitor and used only when the level of the stored energy was adequate to deliver enough power to operate the sensor and the telemetry system. To demonstrate the utility of the power management system, we first used a commercially available temperature sensor, transmitter and receiver, and transmitted the measured temperature data wirelessly from the sensor to a remote receiver. The sensor used was a thermocouple provided by the vendor. When the microbial fuel cell charged the ultracapacitor to 1.2 V, the DC-DC converter was activated to produce a 3.3V output; which was then applied to the transmitter/sensor. After the temperature data was acquired by the transmitter, it was wirelessly transmitted to the receiver. During this process the energy in the capacitor was depleted, causing the potential to decrease below 1.2 V. As a result, the system switched to sleep mode until the capacitor potential reached 1.2 V, which activated the system again. Selecting the potential of 1.2 V as the potential at which the system was changed to active mode was arbitrary; the lower the selected potential, the shorter the charging time for the

capacitor. However, the minimum potential at which we could operate our DC-DC converter was 0.9 V, so there was not much room for varying the selected potential.

After this first initial demonstration we decided to implement this power management system to power up a more complicated chemical sensor that was not available commercially. This chemical sensor was prototyped and built by our research team and was designed to detect copper and lead in water. The chemical sensor module was designed to carry out the electro-analytical process of anodic stripping voltammetry to detect copper and lead.

Anodic stripping voltammetry (ASV) is an electrolytic method in which a mercury thin-film electrode is held at a negative potential (-1.1V) to reduce metal ions in solution to form an amalgam with the electrode. The solution is stirred to carry as many of the metal ions to the electrode as possible. After deposition, the potential is scanned from -1.1V to 0.5V at the same time the current drawn by the mercury thin-film electrode is measured. Current peaks appear at potentials corresponding to the oxidation of metals as they are stripped from the electrode back into the solution. The peak height obtained was correlated to the concentration of the metal ions in the solution using previously measured calibration curves.

Just as before, the microbial fuel cell charged an ultracapacitor to 1.2V. As soon as this voltage was reached the DC-DC converter was activated and it was designed to output a voltage of 5V which was needed to power up the chemical sensor module and its sensor. The metal concentration data obtained was then wirelessly transmitted to the receiver which was connected to a data logging PC.

CHAPTER 2

MATERIALS AND METHODS

Components of the System

A block diagram of the telemetry system powered by the microbial fuel cell is shown in Figure 2.1. All electronic components were commercially available from specialized vendors although some had to be modified to fit our needs.

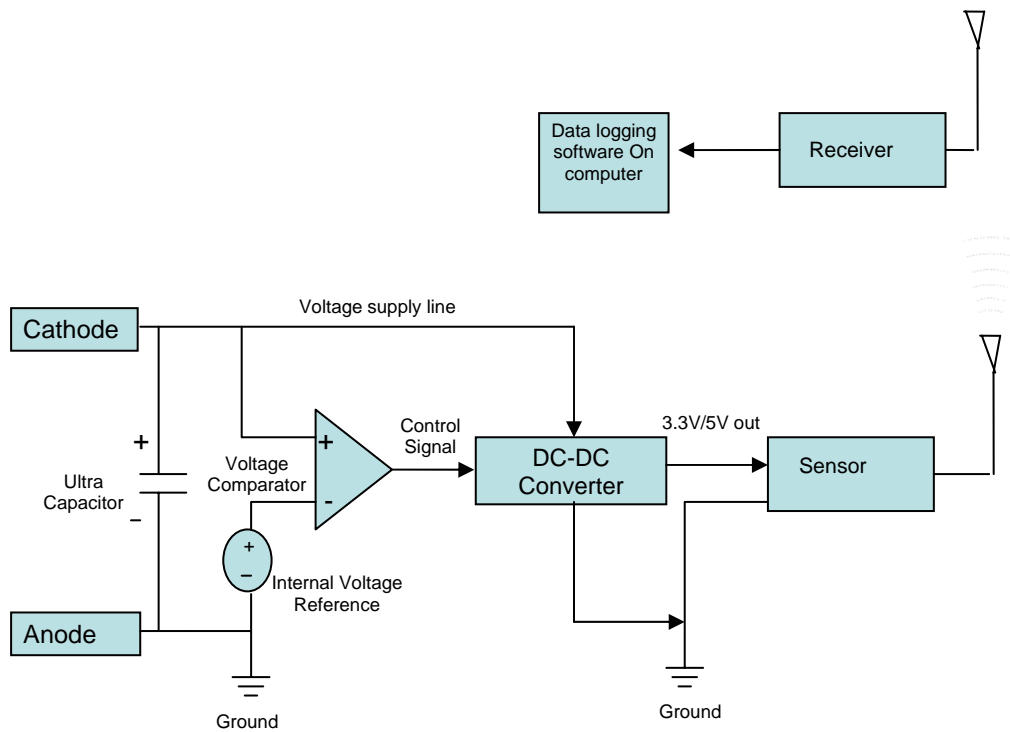


Figure 2.1. Block diagram of the telemetry system powered by the microbial fuel cell.

The Cathode

Figure 2.2 shows the microbial fuel cell cathode that was built to demonstrate that the power management system works. To make the cathode, we used 316L stainless steel wire (0.9mm diameter) electrodes wound in spherical balls (manufactured by J.W. Harris, Mason, OH; part number 0316LF2) with a 1ft² surface area for the temperature sensor and an area of 4ft² for the chemical sensor. The chemical sensor consumed more power compared to the temperature sensor. As a result a higher surface area of cathode was needed. The cell was designed in such a way that the cathode was limiting the short circuit current. Figure 2.2 depicts four 316L stainless steel cathodes that have been wound in spherical balls and then connected together. All four electrodes were encased in a wooded box for submersion into Hyalite Creek; which was the location of the chemical sensor module.

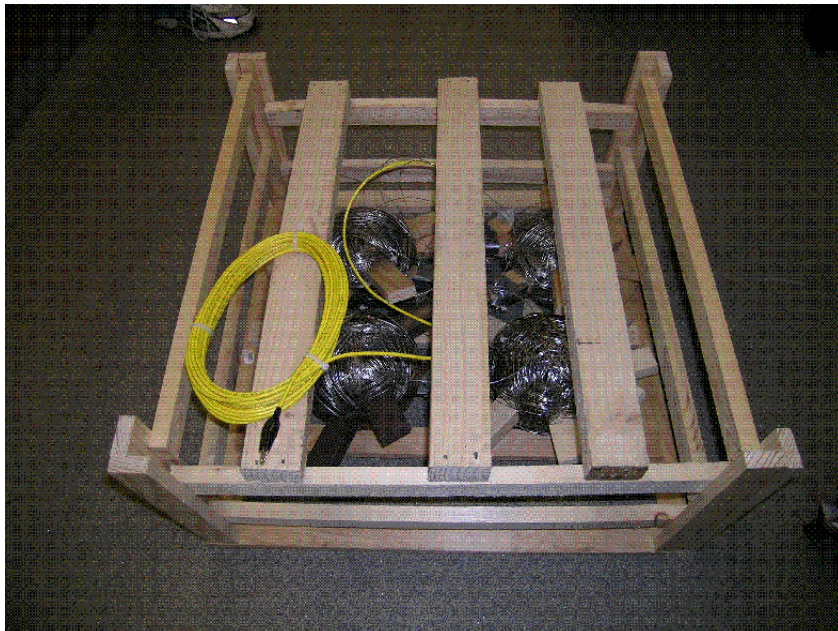


Figure 2.2 Picture of cathodic electrodes deployed in Hyalite Creek.

The Anode

The anodes were made of a magnesium alloy (Farwest Corrosion Control Company, Gardena, CA 90248; IR8 Ultramag high potential magnesium anode); they were cylindrical and each had 265 cm² surface area and weighed 0.45 kg. These anodes deliver up to 500mA of current per 265 cm² of anodic surface area. According to the vendor, the magnesium alloy electrode used in this study contained aluminum 0.01% max, manganese 0.50-1.3%, copper 0.02% max, silicon 0.05% max, iron 0.03% max, nickel 0.001% max, others each 0.05% max, and the remainder, about 99%, was magnesium. The four anodes are pictured in figure 2.3 they have been tie-strapped together for convenience. An anodic surface area of 600 cm² was used for the temperature sensor and 2400 cm² for the chemical sensor module, the higher surface was needed because the chemical sensor consumed more power and a higher anodic surface area is able to deliver more electrons.



Figure 2.3. Four sacrificial magnesium anodes bound together with a tie-strap.

Ultracapacitor

An ultracapacitor was used to store the energy generated by the environmental microbial fuel cell. The ultracapacitor we used for the temperature sensor was manufactured by Maxwell Technologies (9244 Balboa Avenue, San Diego, CA 92123 <http://www.maxwell.com>) and was rated at 4 farad @ 2.5 V. The chemical sensor module consumed more power than the temperature transmitter. As a result we used a higher valued ultracapacitor for energy storage for the chemical sensor module. The ultracapacitor used for the chemical sensor was also manufactured by Maxwell technologies (PC100E); it was rated at 100F @ 2.5V. Figure 2.4 shows three of the ultracapacitors that are available from Maxwell technologies. The 4 farad ultracapacitor was used to power the temperature sensor and the 100 farad ultracapacitor was used to power the chemical sensor. The last ultracapacitor shown is the 350 farad ultracapacitor that was not used for any of the sensors described in this thesis but it can be used for applications that require a higher power output. These ultracapacitors were connected to the anode and cathode using the setup shown in figure 2.1.



Figure 2.4. Ultracapacitors from left to right: 4 farad, 100 farad and 350 farad

DC-DC Converter

The DC-DC converter used to power the telemetry systems was the max1797 manufactured by Maxim Semiconductor (120 San Gabriel Drive, Sunnyvale, CA 94086, www.maxim-ic.com). This DC-DC converter was chosen because it is 95% efficient, draws a low quiescent current of 25uA and the minimum input voltage needed is 0.7V. An “evaluation kit” (max1797evkit) was initially purchased to test the DC-DC converter to make sure it meets all the requirements. An evaluation kit is basically a printed circuit board that contains all the necessary external components needed to operate the DC-DC converter. The max1797evkit is pictured in figure 2.5.



Figure 2.5. Max1797evkit DC-DC converter used to power the temperature sensor.

We modified the DC-DC converter provided by the vendor to:

1. Increase the output potential to 3.3V for the temperature sensor and 5V for the chemical sensor module.
2. Automatically power up the system when the capacitor voltage reached 1.2V (when enough energy was accumulated in the system, the sensor and telemetry system was operated automatically).
3. Keep the output voltage constant for the sensor operation (the potential of our fuel cell varied between 1.55V and 2.2V).

The circuit in Figure 2.6 accepts a variable or constant input voltage in the range of 0.9 V to 5.5V and delivers a stable output at 3.3V to power the temperature sensor.

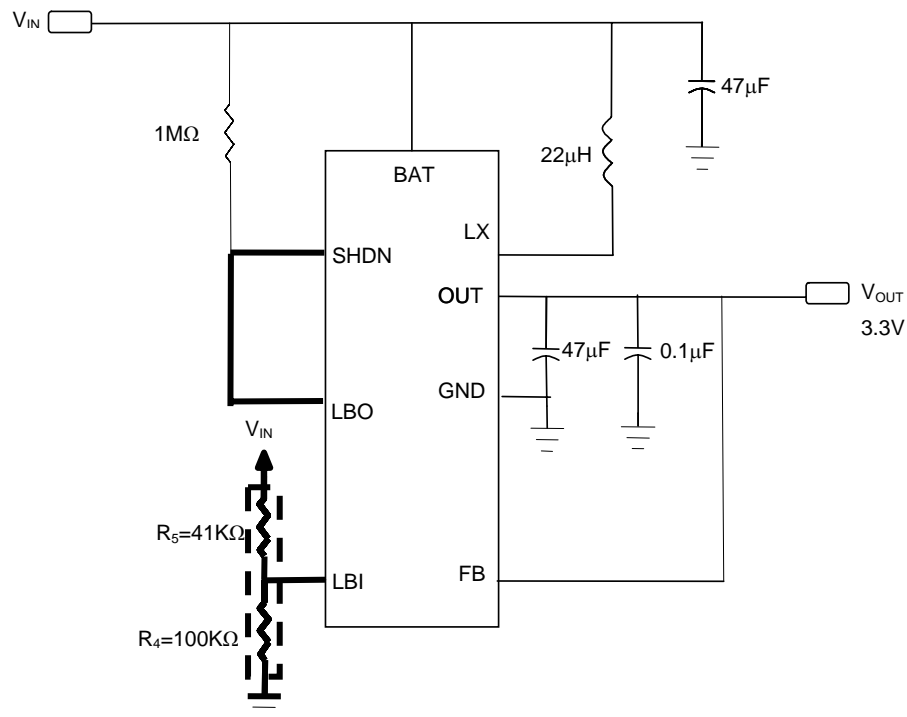


Figure 2.6. The modified DC-DC converter for a 3.3V output used to power the temperature sensor. The modifications are marked with a thicker line.

The chemical sensor module was built exclusively by our research group. All the designed electronic components were prototyped and then a custom printed circuit board (PCB) was manufactured onto which all the components were mounted. This custom chemical sensor module was designed to operate from a 5V power supply as compared to the 3.3V that was used to power the temperature transmitter. Instead of using the evaluation kit offered by maxim semiconductor for the DC-DC converter, we integrated the power management circuitry into the PCB design for the chemical sensor module. The circuit design for the DC-DC converter used to power the chemical sensor module is shown in figure 2.7. Here again the DC-DC converter was set to activate at an input potential of 1.2V.

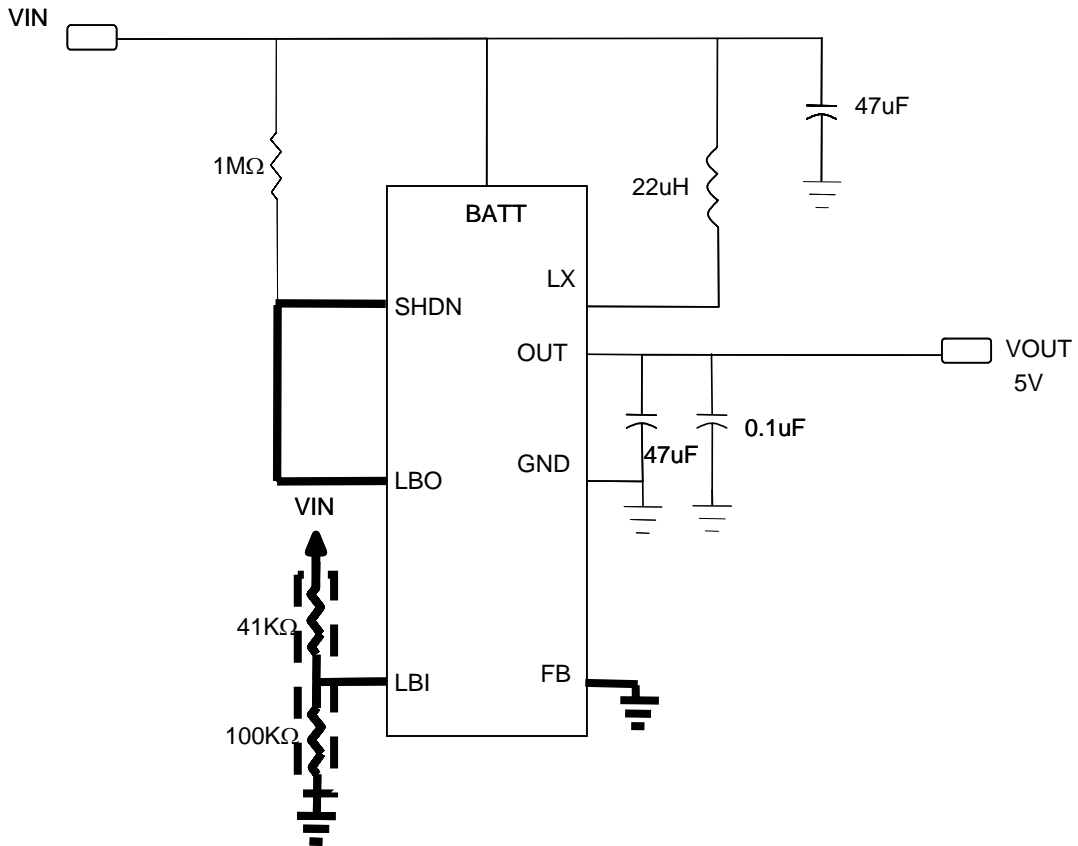


Figure 2.7. The modified DC-DC converter for a 5V output used to power the chemical sensor module. The modifications are marked with a thicker line.

Voltage Comparator

The voltage comparator needed for the proposed power management system is integrated into the max1797 DC-DC converter. A voltage comparator is used to compare the external voltage level against a internal voltage reference and then produce a binary output indicating whether the input voltage had reached the set voltage level. The onboard comparator was activated by removing the connection between the pads of resistor R_5 and inserting resistors R_4 and R_5 , whose values depended upon the voltage chosen to activate the comparator (V_{level}). Choosing R_4 as

100 k Ω and V_{level} as 1.2V, R_5 was 41 k Ω , calculated from the following equation which was obtained from the max1797 datasheet:

$$R_5 = R_4 \left(\frac{V_{\text{level}}}{0.85} - 1 \right) \quad (5)$$

After resistors R_4 and R_5 were inserted onto the board, the low battery output (LBO) pin was connected to the SHDN pin, enabling the voltage comparator and thus completing the circuit. The shutdown SHDN pin acted as an on-off switch for the output. Applying a voltage higher than 1.2 V to the SHDN pin forced the device into shutdown and when the SHDN pin was grounded, the device was activated. The voltage level on the SHDN pin was controlled by the voltage comparator, which was built into the chip.

The anode and cathode of the microbial fuel cell were connected to pins V_{IN} and GND, respectively, and V_{OUT} and GND were connected to the positive and negative pins of the temperature transmitter/chemical sensor module, respectively.

Temperature Sensor

Temperature Transmitter

The transmitter we used was an off-the-shelf thermocouple/transmitter /receiver kit manufactured by MadgeTech, Inc. part # RFTC4000 for the transmitter

(201 Route 103 West, P.O. Box 50, Warner, NH 03278; www.madgetech.com/index.php). It transmits at a frequency of 418 MHz and has a maximum transmission distance of 100 ft. This temperature transmitter is pictured in figure 2.8. The transmitter was manually activated using a push-button switch. Later on, the system restarted automatically when the fuel cell potential went above (active mode) or below 1.2 V (sleep mode). The push-button switch was connected directly to the ground, allowing the transmitter to be activated when the DC-DC converter was turned on. When needed, the transmitter could be set to operate at predefined time intervals, for example, every 30 minutes. In our setup, the frequency of data transmission was dependent upon the power generated by the microbial fuel cell and the energy stored in the capacitor. When there was not enough energy, the data acquisition and transmission were delayed, and the system waited in sleep mode, until the capacitor was charged.

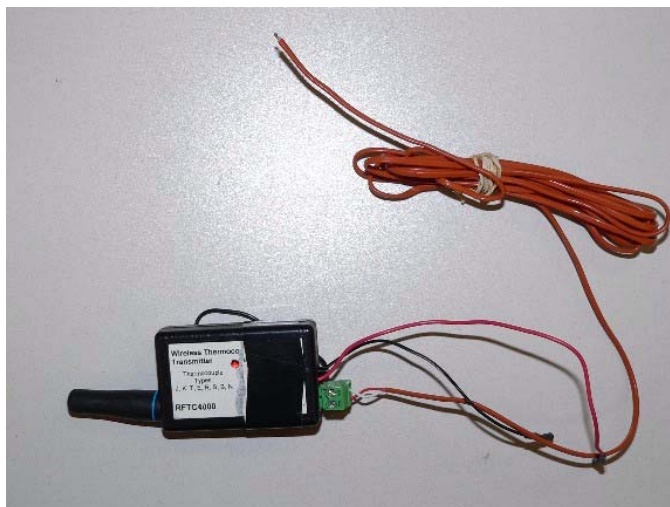


Figure 2.8. RFTC4000 temperature transmitter connected to it is the J-type thermocouple

Remote measurement of the temperature

To demonstrate that microbial fuel cells, when combined with a suitable power management program, can deliver enough energy to operate the temperature sensor and the telemetry system and that our power management system worked as expected, we assembled the system (figure 2.3), connected it with a thermocouple, measured the temperature, and transmitted the data to a remote receiver. The thermocouple, the temperature measurement unit, and the transmitter were powered from the microbial fuel cell. To generate energy, we assembled a microbial fuel cell and deployed it in a freshwater creek, Roskie Creek in Bozeman, Montana. First we deployed stainless steel coupons of 1ft² surface area (the cathodes) and waited until their potential increased above 300 mV_{SCE}. Then we deployed the magnesium alloy sacrificial anode (600cm² surface area), assembled the fuel cell, and connected it to the system shown in figure 2.3.

For demonstration purposes, we measured air temperature and transmitted the data to a remote receiver. The receiver was connected to a laptop computer (IBM T41) located at a distance less than 100 ft from the transmitter. To verify that the measured and transmitted data were correct, we also measured the air temperature using a mercury thermometer and compared the results. To vary the measured temperature and to see if the system responded, we occasionally placed the thermocouple in a beaker filled with ice.

Chemical Sensor Module

The chemical sensor module was designed and constructed by our research team to detect the concentrations of metals such as copper and lead in water. In order to determine whether the chemical sensor was able to accurately measure concentrations of copper and lead we tested this chemical sensor in the laboratory with known concentrations of copper and lead. The chemical sensor module had three ports for the connection of the chemical sensor which consists of the mercury plated working electrode, a platinum counter electrode and a saturated calomel reference electrode. The main component of this sensor module is the microcontroller that was programmed to carry out all the necessary electrochemical operations needed to detect the metals in water. Once the voltage across the ultracapacitor reached 1.2V the onboard DC-DC converter was activated and output a 5V that was used to power all the necessary components of the chemical sensor module.

This chemical sensor performed the electro-chemical process of anodic stripping voltammetry. This procedure required the chemical sensor module to apply a deposition potential of -1.1V to the working electrode to deposit all the metal ions present in the water to the mercury plated working electrode. This deposition potential was applied for a period of 2 minutes followed by the ramping of the potential from -1.1V to 0.5V in order to strip the metals from the electrode. The current drawn by the working electrode was continuously measured by the chemical sensor module during this ramping stage. The current versus potential data obtained

was wirelessly transmitted to our custom-designed receiver module which was powered by a 9V battery. The receiver was also designed with a serial port to be connected to a computer for data download and analysis.

The current vs. ramping potential data was then decoded by Matlab and the results were plotted for further analysis. With our setup the maximum transmission distance was 200 meters but if we were to implant directional antennas we could increase the transmission distance. For all our tests the receiver was placed between 150-200 meters away from the transmitter. Once the analysis was completed the sensor module entered sleep mode. A picture of the chemical sensor transmitter module is shown in figure 2.10 and the receiver is pictured in figure 2.11. The major components of the transmitter and receiver have been indicated in the pictures.

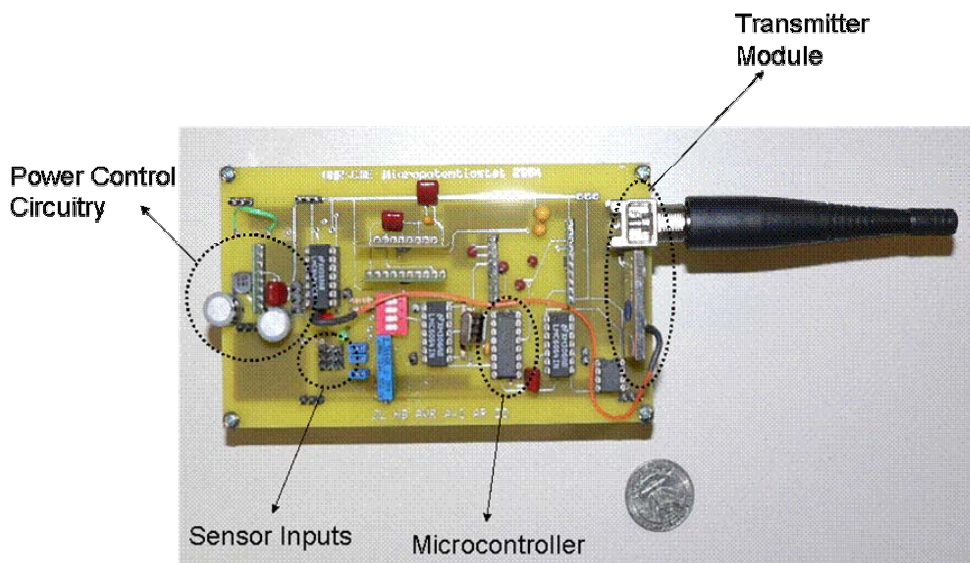


Figure 2.10. Transmitter module, a quarter is placed in this figure to give the reader a sense of scale.

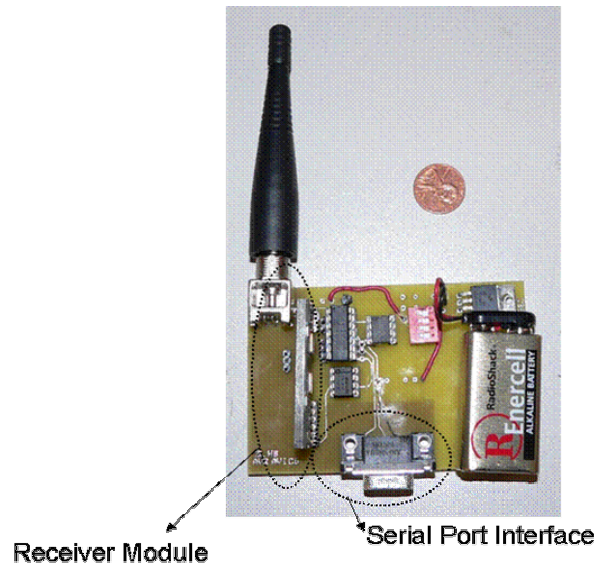


Figure 2.11. Receiver module a penny is placed in this figure to give the reader a sense of scale.

CHAPTER 3

RESULTS AND DISCUSSION

Fuel Cell

We assembled the system step-by-step, starting from the fuel cell. The 316L stainless steel plates used to deposit biomineralized manganese oxides exhibited an initial potential of $-50 \text{ mV}_{\text{SCE}}$, and after approximately 2-3 weeks exposure to the creek water the potential increased to almost $+400 \text{ mV}_{\text{SCE}}$, which is consistent with our previous observations (23), and with thermodynamic calculations (equation 4 page 6). After the cathodic potential reached the desired level of $+400 \text{ mV}$, we deployed the magnesium alloy sacrificial anodes, connected the microbial fuel cell to the circuit in figure 2.3 and left it for three weeks. During that time, the potential of the sacrificial anode varied between -1.6 and $-1.8 \text{ V}_{\text{SCE}}$. We ascribe the variations in anode potential to the fluctuations in the ambient temperature and changing chemistry of the water.

To evaluate the amount of energy generated by the microbial fuel cell, we measured the short-circuit current (by directly connecting the anode to the cathode) of the fuel cell. The short circuit current was measured using a multimeter. To make sure that the cathodic reaction was limiting the current, we increased the number of anodes (i.e., the surface area) until the current reached a plateau. The plot of the measured

current versus the number of sacrificial anodes is shown in figure 3.1, which shows that the cell current was limited by the cathode when the anode surface area exceeded 600 cm^2 (which was equivalent to 0.9 kg of the anode). When the cell was short-circuited, the entire measured current was caused by the dissolution of the sacrificial anode on one side and reduction of the biomineralized manganese oxides on the other side of the cell. The cell was designed so that the current was limited by the cathodic reaction. During the pseudo-steady state (lasting for about 10 minutes) the current was 14 mA, and the current density with respect to the surface of the cathodes was $3.9 \mu\text{A}/\text{cm}^2$. The short-circuit current was almost constant for over 10 minutes, and then it was slowly decreasing at a rate of 0.1 mA during 10 minutes. We explain the existence of the pseudo-steady state by the microbiology stimulated recycling of the cathodic reactant, MnO_2 .

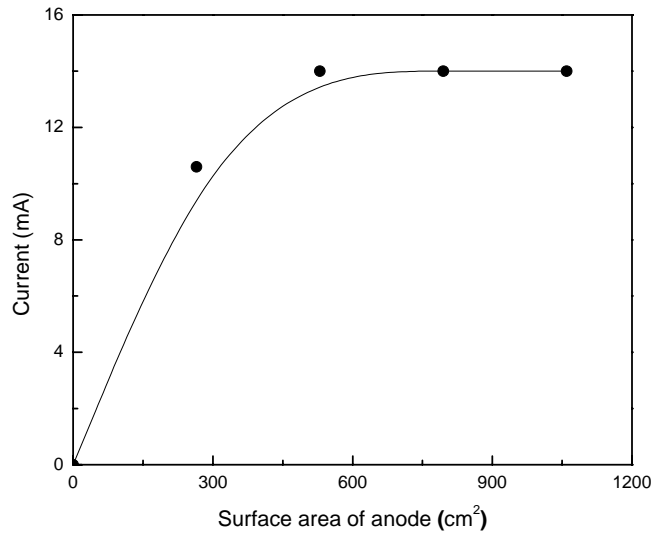


Figure 3.1. Cell current versus anodic surface area.

Charging the Capacitor and Starting the System

A charge curve for the capacitor is shown in Figure 3.2. When the potential of the fuel cell reached 2.1 V, we connected the 4 Farad capacitor (used for the temperature sensor) to the circuit to measure the capacitor charge curve, shown in Figure 3.2. Immediately after connecting the capacitor, the potential of the cell dropped to zero because the uncharged capacitor acted like a short circuit in the system. However, over time, the potential of the system slowly increased, showing the ability of the fuel cell to charge the capacitor.

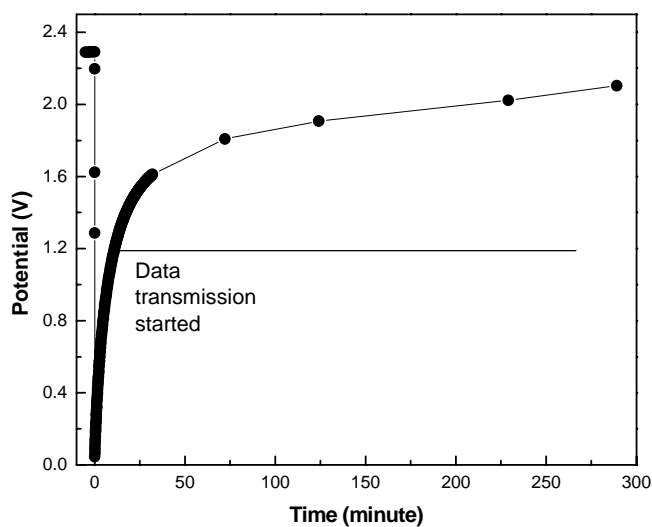


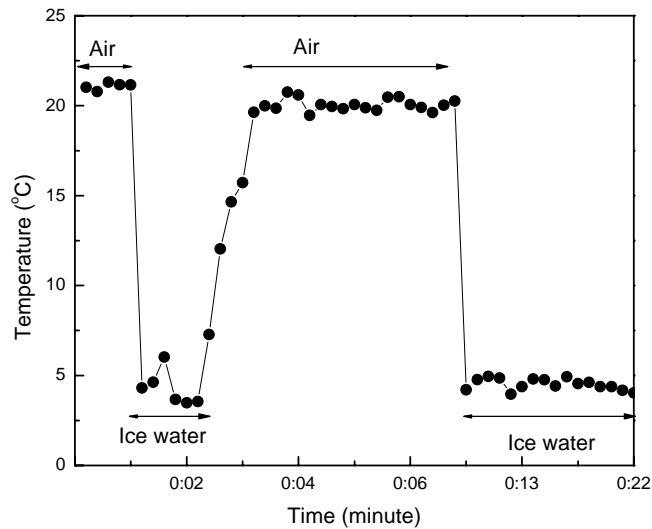
Figure 3.2. Capacitor charge curve obtained from the microbial fuel cell deployed in Roskie Creek.

Once the capacitor was charged above 1.2 V, our telemetry system was automatically activated and transmitted the measured temperature wirelessly. The selection of 1.2 V for starting the telemetry system was arbitrary. A different level

could be selected: the lower the selected potential, the shorter the charging time for the capacitor. Examples of the transmitted data are shown in figure 3.3.

First Example Application: Remote Measurement of Temperature

To test the telemetry system, we measured the ambient air temperature and then inserted the thermocouple into cold water and measured the temperature again. This cycle was repeated several times (figure 3.3). During these tests the entire system was powered by the microbial fuel cell. The readouts were wirelessly transmitted from the thermocouple via the transmitter to the receiver (the computer).



Second Example Application: Remote Measurement of
Copper and Lead Concentration

Just as with the temperature sensor, the same procedure was used for the chemical sensor. Once the 100 Farad capacitor was charged to 1.2V the chemical sensor module automatically turned on and it carried out the electro-chemical analysis of the water. The chemical sensor was built to detect lead and copper concentrations but as the waters around Bozeman are extremely pristine we could not test the sensor in the field, instead we connected the sensor module to the sensor in the laboratory and carried out the analysis with water that contained known concentrations of copper and lead.

Figure 3.4 depicts the output from the receiver module. The two curves are for two different concentrations of lead and copper. The first peak indicates the detection of lead and the second peak corresponds to copper. Initially the solution contained 2ppm of copper and lead and the stripping process was carried out. The grey curve in figure 3.4 corresponds to this concentration. The analysis was then repeated by increasing the concentration of copper and lead to 2.5ppm and the stripping process was repeated. The black curve in figure 3.4 corresponds to this concentration. The peak heights can be correlated to the concentration using calibration curves and figure 3.4 shows us the increase in peak height that corresponds to the increase in metal ion concentration from 2ppm to 2.5ppm

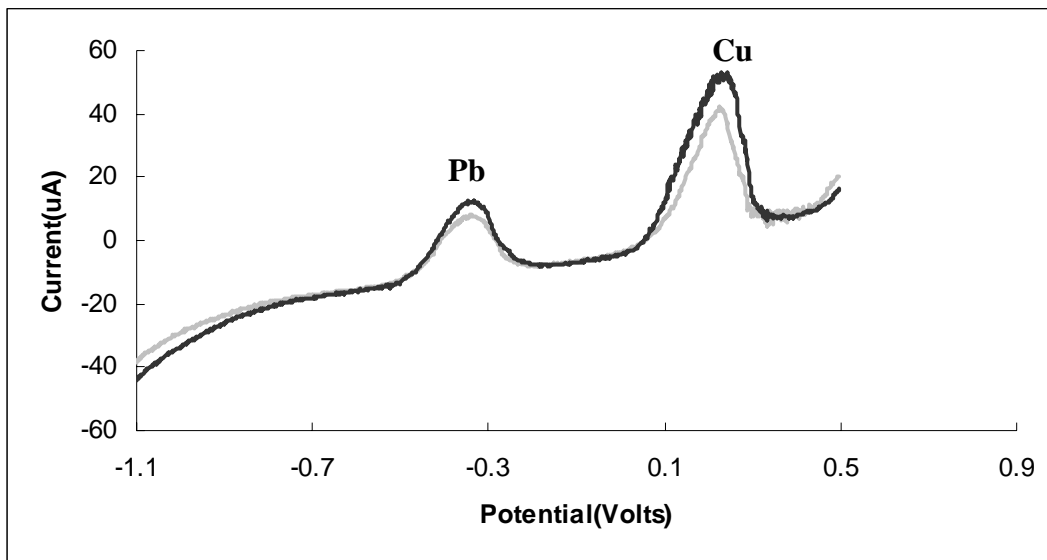


Figure 3.4. Data transmitted from the chemical sensor module, the peaks shown indicate the detection of copper and lead. The grey curve is a concentration of 2ppm and the black curve is at a concentration of 2.5ppm for lead and copper. The chemical sensor module was powered using the environmental microbial fuel cell.

Power Needed for the Chemical Sensor Module

During one cycle of the chemical sensor module a data logger was connected to the module to measure the amount of current that was drawn by the chemical sensor. The output from the logger is shown in figure 3.5. The increase in current at about 5.5 minutes is contributed to the transmitter module being activated to wirelessly transfer the data obtained to the receiver. The chemical sensor module draws an average of 80mA over a period of 7 minutes for one electrochemical

analysis. Therefore the power that is needed by the chemical sensor module for one electrochemical analysis is $P=0.08A*5V=0.4Watts$.

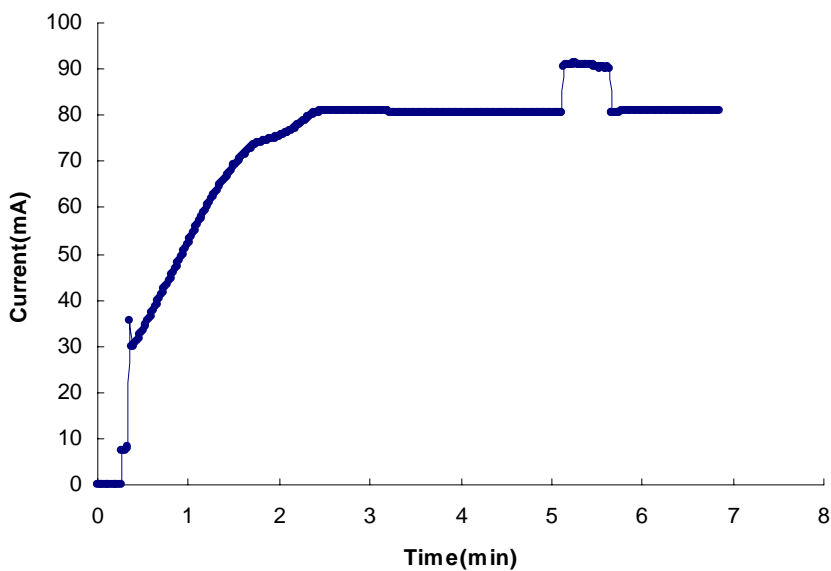


Figure 3.5. Current drawn by the chemical sensor module over time for one electrochemical analysis.

Limitations of the system

It is important to estimate how long the entire system, the microbial fuel cell, the sensor, and the telemetry system, may last. This may be estimated by predicting the lifetime of the components. The lifetime of the cathodic side of the fuel cell, 316L stainless steel, should not be the limiting factor as long as there is microbial growth

and oxygen. Assuming that the life-time of the fuel cell is limited by the life time of the anode, it can be calculated from the current required to power the telemetry system and the temperature sensor. Using data available from the manufacturer of the temperature transmitter system and the sacrificial anodes we estimate that approximately 0.015 A is required to measure temperature and transmit data every 8 seconds. The ampere-hour rating of the anodes varies with environmental conditions; a 0.45kg (265-cm² initial surface area) magnesium anode can be rated at about 500 ampere-hour (Farwest Corrosion Control Company, Gardena, CA 90248). Therefore, for 600 cm² of anode surface area it is rated at 1000 ampere-hour. Based on that, the lifetime of the microbial fuel cell is estimated as: Lifetime (h) with 0.45 kg of anode = $1000\text{Ah}/(0.015\text{A}) = 66666 \text{ h} = 7.61 \text{ years}$. The same calculation can be done for the chemical sensor module which draws 0.08A for approximately 7 minutes. But for the chemical sensor we used 4ft² of cathodic surface area which corresponds to an anodic surface area of 2400 cm². This leads to a lifetime of $4000\text{Ah}/(.08\text{A}) = 5.703 \text{ years}$. If needed, these numbers can be increased just by increasing the numbers of anodes.

The calculated lifetime depending on the number of the anodes and the current needed to operate the system is hypothetical and the actual lifetime may vary depending on environmental conditions. For example, one unknown factor is the rate of corrosion of the sacrificial anodes, and that can be evaluated by running long-term tests. However, the lifetime of the anode in this fuel cell can still be controlled by increasing the surface area of the anode.

The lifetimes of the telemetry system and the temperature sensor are limited by the lifetime of the capacitor, which was listed by the vendor as 10 years. Also, the telemetry system and temperature system may break down before the capacitor loses its ability to charge and discharge, or the anode dissolves completely. Altogether, if carefully designed and protected when deployed, the system can last for years.

CHAPTER 4

CONCLUSION

In summary, several studies have shown the possibility of harvesting energy from the environment using microbial fuel cells, such as harvesting energy from marine sediments. However, to the best of our knowledge, none of these studies have demonstrated applications of microbial fuel cells. Our study is the first attempt to use microbial fuel cells to power two different kinds of sensors with a telemetry system that transmits the measured data wirelessly.

In the first step, we used our power management circuitry to use the energy generated by an environmental microbial fuel cell to power a thermocouple-based temperature sensor. This was successfully demonstrated and the temperature data were transmitted to a remote receiver. In the second step, we used the same setup to power a chemical sensor module and the sensor itself. This system was again successfully tested in the field but since there is close to no copper and lead in the waters around Hyalite Creek we tested the chemical sensor module in the laboratory with known concentrations of copper and lead. The data obtained by the chemical sensor module were successfully transmitted wirelessly to the receiver. These demonstrations prove that with the implementation of our power management circuitry it is possible to power various kinds of sensors and telemetry systems using environmental microbial fuel cells.

Using the proposed power management system, future researchers can deploy various microbially powered sensors. Long-term testing of this system was not carried out in this study, but will need to be done to determine the long term reliability of this system in the environment. Further improvements such as the design of a custom DC-DC converter that is able to boost voltages as low as 0.3V-0.5V to 5V can be implemented with higher powered transmitters so these sensors can be deployed in remote locations to monitor environmental parameters.

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